

Lab on a Chip

Accepted Manuscript



This article can be cited before page numbers have been issued, to do this please use: G. Li and D. Lee, *Lab Chip*, 2017, DOI: 10.1039/C7LC00768J.



This is an Accepted Manuscript, which has been through the Royal Society of Chemistry peer review process and has been accepted for publication.

Accepted Manuscripts are published online shortly after acceptance, before technical editing, formatting and proof reading. Using this free service, authors can make their results available to the community, in citable form, before we publish the edited article. We will replace this Accepted Manuscript with the edited and formatted Advance Article as soon as it is available.

You can find more information about Accepted Manuscripts in the [author guidelines](#).

Please note that technical editing may introduce minor changes to the text and/or graphics, which may alter content. The journal's standard [Terms & Conditions](#) and the ethical guidelines, outlined in our [author and reviewer resource centre](#), still apply. In no event shall the Royal Society of Chemistry be held responsible for any errors or omissions in this Accepted Manuscript or any consequences arising from the use of any information it contains.



Lab on a Chip

PAPER

Advanced selective liquid-metal plating technique for stretchable biosensor applications†

Guangyong Li^{a, b} and Dong-Weon Lee^{*b}

Received 00th January 20xx,
Accepted 00th January 20xx

DOI: 10.1039/x0xx00000x

www.rsc.org/

This paper presents a novel stretchable pulse sensor fabricated by the selective liquid-metal plating process (SLMP), which can conveniently attach to human skin and monitor the patient's heartbeats. The liquid metal-based stretchable pulse sensor consists of polydimethylsiloxane (PDMS) thin films and liquid metal functional circuits with electronic elements that are embedded into the PDMS substrate. In order to verify the utility of the fabrication process, various complex liquid-metal patterns are achieved by using the selective wetting behavior of the reduced liquid metal on the Cu patterns of the PDMS substrate. The smallest liquid-metal pattern is approximately 2 μm in width with uniform surface. After verification, a transparent flowing LED light with programmed circuits is realized and exhibits stable mechanical and electrical properties under various deformations (bending, twisting and stretching). Finally, based on the SLMP, a wireless pulse measurement system is developed which is composed of the liquid metal-based stretchable pulse sensor, a Bluetooth module, an arduino development board, a laptop computer and a self-programmed visualized software. The experimental results reveal that the portable non-invasive pulse sensor has the potential to reduce costs, simplify biomedical diagnostic procedures and help patients to improve their life in future.

Introduction

The monitoring of vital signs is an effective way for physicians to assess the status of essential functions of human body in modern medical care and diagnosis.¹ These physiological signals in the biological system can be accurately monitored and recorded using the various medical system.^{2, 3} In general, the real-time monitoring process of the vital signals is complex and require experienced personnel. Sensors employed in current systems also show limited flexibility and stretchability when they are mounted on human bodies. Traditional monitoring techniques have several advantages in early diagnosis for patients, but are limited to those widely used due to the high mechanical stiffness of the sensor. With attractive properties such as biocompatibility, light weight and transparency, the development of stretchable sensors that monitor the changes in human beings with a vital sign such as temperature, blood pressure, breathing rate etc. have great interest from the scientific community.⁴ In recent years, a variety of innovative manufacturing technologies have been developed to meet market requirements in stretchable electronics. These sensors are integrated with tiny electronic

components that can be adhered onto non-planar skin of human.^{5–13} In the early stages of the development for flexible electronics, thin films patterned with deterministic geometries or conductive particles in elastomer have been widely used to minimize changes in electrical properties.^{11–13} Although these techniques are very suitable for flexible electronics, it is not easy to apply them to stretchable electronics.¹⁰ Compared to other methods, liquid metals can only be categorized as intrinsically stretchable because they are softer than common materials used for flexible electronics. The most efficient technology for stretchable electronics is to print liquid metals on an elastomeric substrate. Various liquid-metal printing techniques such as stencil mask-based printing,^{14, 15} injecting,^{16–20} atomized spraying,^{21–23} direct writing,^{24–29} masked deposition,³⁰ and inkjet printing³¹ have been developed to realize flexible and stretchable electronics. For injecting technique, the microfluidic channel injected with liquid metal can be utilized for the electrical interconnector in the applications of stretchable RF radiation sensor, capacitors, inductors and liquid metal-based electrical interconnector.^{16–20} The resolution of liquid metal pattern fabricated by injecting technique is depended on the resolution of microfluidic channel. The max strain of liquid metal-based electrical interconnector can be up to ~600%.²⁰ Nevertheless, when the size of microfluidic channel is decreased below 20 μm , the oxidized liquid metal is difficult injected to the nozzle. Due to the extra demand of the needle and syringe for liquid metal injecting, this manual method takes some drawbacks in geometry and high-volume manufacturing. For other techniques mentioned above, the low resolution (pattern planar dimension >100 μm)

^aFaculty of Mechanical Engineering and Mechanics, Ningbo University, Ningbo, 315211, China.

^bMEMS and Nanotechnology Laboratory, School of Mechanical Engineering, Chonnam National University, Gwangju, 61186, South Korea. E-mail: mems@chonnam.ac.kr; Fax: +82 62 5301684; Tel: +82 62 5301689.

†Electronic Supplementary Information (ESI) available: [details of any supplementary information available should be included here]. See DOI: 10.1039/x0xx00000x

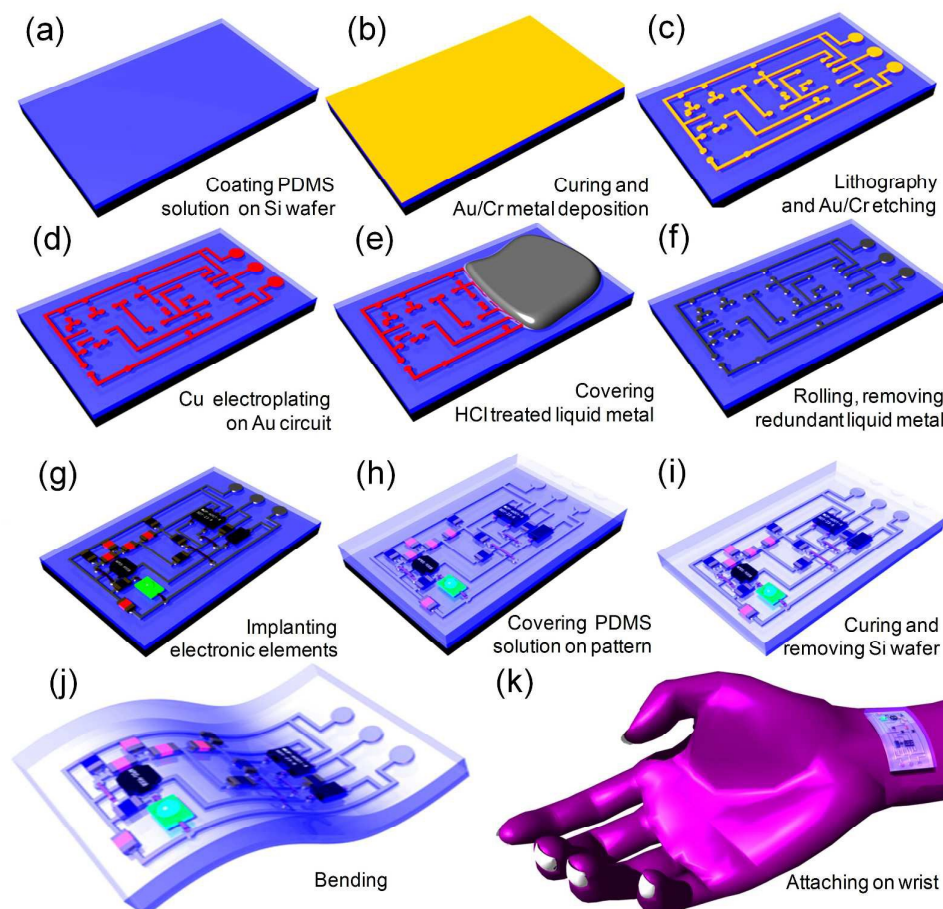


Fig. 1. Fabrication process of the liquid-metal-based stretchable pulse sensor; (a) Spin-coating of PDMS solution onto a Si wafer. (b) PDMS curing, oxygen plasma treatment, and Au/Cr (100 nm/10 nm) deposition using an electron-beam (e-beam) evaporator. (c) Photolithography and Au/Cr etching. (d) Cu electroplating (2 μm) on Au pattern. (e) Dropping HCl-treated liquid-metal onto the adhesion patterns. (f) Rolling of the liquid-metal droplet over the PDMS substrate and removing the excess liquid-metal droplet. (g) Implanting electronic elements on liquid-metal circuit. (h) Covering the liquid-metal pattern with a PDMS solution. (i) PDMS curing and separation of the Si wafer. (j) Bending test. (k) Attaching the circuit onto the wrist.

and irregular edge of printed liquid metal patterns provide limits to meet the demands of stretchable electronics. A lift-off technique is also applied to liquid metals by spreading the metal onto substrates covered by photoresist patterns and then dissolving away the photoresist, leaving behind only the liquid metal in contact with the substrate. This technique allows to form liquid metal patterns with about 20 μm features. Even though a variety of excellent methods have been developed, the technology for reliably forming liquid metal patterns of several micrometers in a large area still remains as a challenge. Biocompatibility of the stretchable sensors is also one of important considerations in design and fabrication processes.

Herein, we developed a stretchable biosensor platform (liquid metal-based stretchable pulse sensor) that use an advanced selective-liquid metal plating (SLMP) process to

enable comfortable monitoring of a patient's condition for personal healthcare. The SLMP process is mainly based on the selective wetting behaviour of hydrochloric acid (HCl)-treated Galinstan (gallium–indium–tin liquid alloy) on various thin film surfaces. To summarize briefly, the reduced Galinstan droplets are in contact with the metal patterns (Au/Cr pattern) and the polydimethylsiloxane (PDMS) substrate, respectively, exhibiting superlyophilic and superlyophobic characteristics (described in Fig. S1 of the ESI†). The superlyophilic characteristic of metal materials allows the selective plating of Galinstan on the metal-patterned PDMS surface. However, the corrosion of a thin Cr layer to HCl-treated Galinstan greatly affects the uniformity of the liquid-metal patterns and this restricts the high resolution (shown in Fig. S2 of the ESI†). More details of the SLMP process have been discussed in our previous works.^{32–36} In order to improve the uniformity and

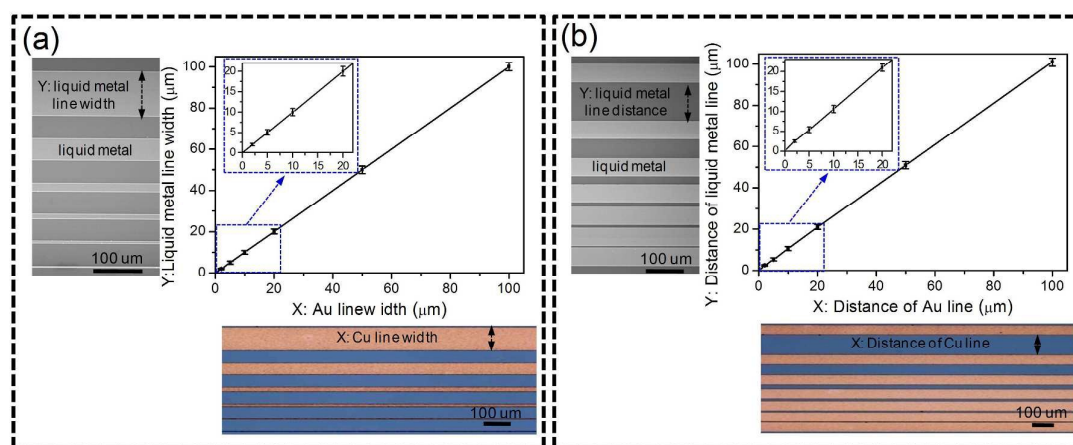


Fig. 2. SEM and optical images of liquid-metal; the plots of (a) width of the liquid-metal lines versus the width of Cu lines, and (b) the length of the liquid-metal lines versus the lengths of the Cu before liquid-metal plating. The width and length of liquid-metal lines vary in the range from 2 μm to 100 μm .

avoid the corrosion issue between the Cr layer and the HCl-treated Galinstan, Au/Cr patterns are covered with a Cu thin layer. This is because HCl acid does not react with Cu. Only metals whose standard reduction potential is lower than the standard reduction potential of hydrogen react with non-oxidizing acids such as HCl and diluted H_2SO_4 to displace hydrogen. As a result, the minimum line width that can be realized is greatly improved.

Results and discussion

Principle of liquid-metal-based stretchable pulse sensor

In modern medical treatment and diagnosis, several methods such as electrocardiography (ECG), photoplethysmography (PPG), etc have been developed for measuring heart rate. Of these heart rate monitoring methods, the ECG is widely used as a standard diagnostic technique. However, the ECG technique requires specialized equipment and has diagnostic limitations that restricts on patients' activities. This method also causes uncomfortable emotions from the physiological and psychological point of view. The PPG technique is a non-invasive, inexpensive, reliable and low power consuming optical technique that makes it easier to monitor a patient's pulse compared to the ECG. In the PPG technique, the pulse rate can be easily monitored from the change in the transmittance induced by blood pressure when the light from a light-emitting diode (LED) illuminates the human skin. However, limited flexibility and stretchability remain as a drawback of the PPG technique. Therefore, we proposed a new method of fabricating a flexible pulse sensor based on liquid metal as shown in Fig. 1 by combining the principle of PPG and the improved SLMP technology. The pulse sensor is a kind of reflection-type photoelectric sensor and is composed of a light source (LED) and a photoelectric converter (schematic diagram shown in Fig. S3 of the ESI†). Because arterial blood oxygen and hemoglobin are sensitive to light in the wavelength range of 500 nm to 700 nm, a green LED with a wavelength of about 560 nm is used as the light source. During each

cardiac cycle, the green light illuminates the blood vessel under the skin of a person and the blood volume in the arterial blood vessels changes periodically, causing a change in the transmittance. The reflected light from blood vessel cells is measured by a photo sensor and transferred to electrical signals with the help of the photoelectric converter (model: APDS-9008). To avoid any influence by environmental noise, a low-pass filter and an operational amplifier (model: MCP6001) are integrated with the stretchable biosensor platform.

Liquid-metal pattern embedded in PDMS

In order to verify the applicability of the improved SLMP technique for stretchable or flexible electronics, various liquid-metal patterns with different widths and gap distances are demonstrated as shown in Fig. 2. As can be seen in Fig. 2(a), the first test pattern includes liquid-metal lines with a width in the range of 2 μm to 100 μm on a substrate. Each liquid-metal line is spaced with edge-to-edge separations of 50 μm . Next, liquid-metal lines having a line width of 50 μm are formed on a substrate as shown in Fig. 2(b). The edge-to-edge separations in the line arrays are in the range of 2 μm to 100 μm . As mentioned in our previous works,³⁶ the concentrations of HCl solutions and the rolling time of the reduced liquid-metal over metal patterns significantly affect the uniformity of the liquid-metal pattern, especially to the edge of the patterns. This is due the chemical reaction between diluted-HCl and thin Cr patterns (shown in Fig. S2a1, b1, c1 of the ESI†). This can be improved by changing the existing SLMP process. The uniform liquid-metal patterns fabricated using the improved SLMP technique show better pattern edges, even for the smaller liquid-metal lines with a width of 2 μm (shown in Fig. S2a2, b2, c2, of the ESI†).

Fig. 3(a–b) shows microscale alphabet and micro-flower patterns successfully generated on a silicon dioxide surface. This method ensures improved uniformity of the liquid metal pattern edge even at different types of sizes. The minimum width of liquid-metal patterns is less than 2 μm . The complex liquid metal patterns are

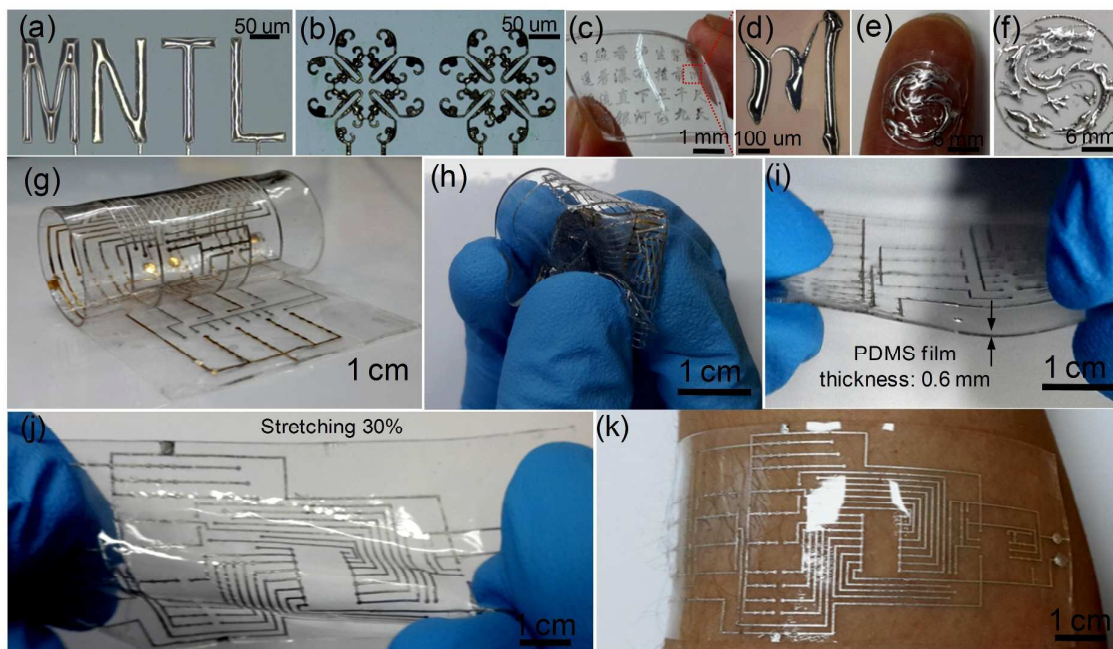


Fig. 3. Complex patterns of liquid-metal plated on silicon dioxide surface and embedded in PDMS with different patterns; (a) Microscale alphabet, (b) Flower, (c–d) Chinese characters, and (e–f) Dragon. Complex liquid-metal circuit embedded in the thin PDMS film with (g) crimping and (h) crumpling deformation, (i) 600- μm -thickness, and (j) stretching deformation. (k) Attached the circuit onto the skin of the arm for demonstration.

embedded in PDMS film that includes Chinese characters and dragon patterns as shown in Fig. 3(c–f), demonstrating the versatility approach to rapidly fabricate liquid-metal-patterns with a milli-to-microscale resolution over a large area. The liquid metal-based complex circuit embedded in the PDMS thin film (with a 600- μm thickness) can be bent or stretch arbitrarily when attached to human skin (Fig. 3(c–k)). In addition, the transparency of the flexible sensor exceeds 95% in the visible light range. Although the circuit made of liquid metal embedded in the PDMS is not transparent, it almost has no influence to the transparency of the flexible electronics when the line width of circuit is < 100 μm .³⁶ The stretchability can be easily improved by employing Ecoflex (platinum-catalyzed silicone rubber) as a substrate.

Application of liquid-metal-based stretchable pulse sensor

After demonstrating the functionalities of the improved SLMP technique, we realized practicality by implementing transparent LED circuits, shown in Fig. 4(a–d). Fabrication processes of the LED circuit are similar to the pulse sensor except the integrated electronic elements. As discussed in earlier works,³⁶ the change in resistance of stretchable liquid-metal wires seriously affect to the electrical characteristics of the sensor when the widths of liquid-metal lines is less than 50 μm . If the wire width is greater than 50 μm , the resistance change can be ignored even after 100% stretching. In order to maintain the stable electrical performance for stretchable electronics, we applied “S”-shaped liquid-metal wires instead of straight lines during the fabrication. The resistance

changes of the S-shaped liquid-metal wire (wire width: 5 μm , straight length: 10 mm) is less than 30% after 100% stretching as shown in Fig. 4. In addition, the stretchable circuit can be self-healed electrically at ambient conditions when they are damaged by something sharp. This is due to the liquid characteristics of the electrical wires.

Fig. 5(a) shows an example of stretchable electronic platforms using the advanced SLMP method. To simplify the fabrication process, we employed an embedded liquid-metal wire with a wire

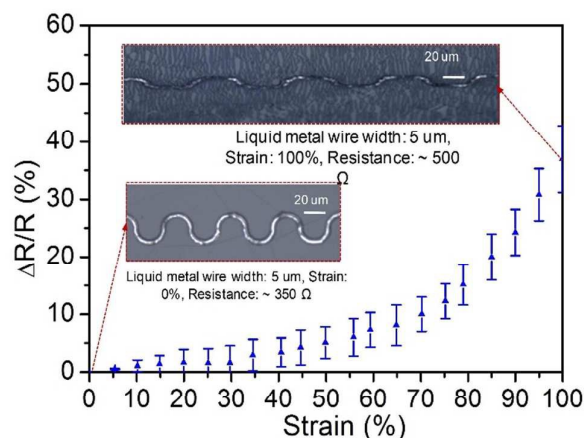


Fig. 4. Electrical characterization of liquid-metal wire with “S” shape (wire width: 5 μm , straight length: 10 mm).

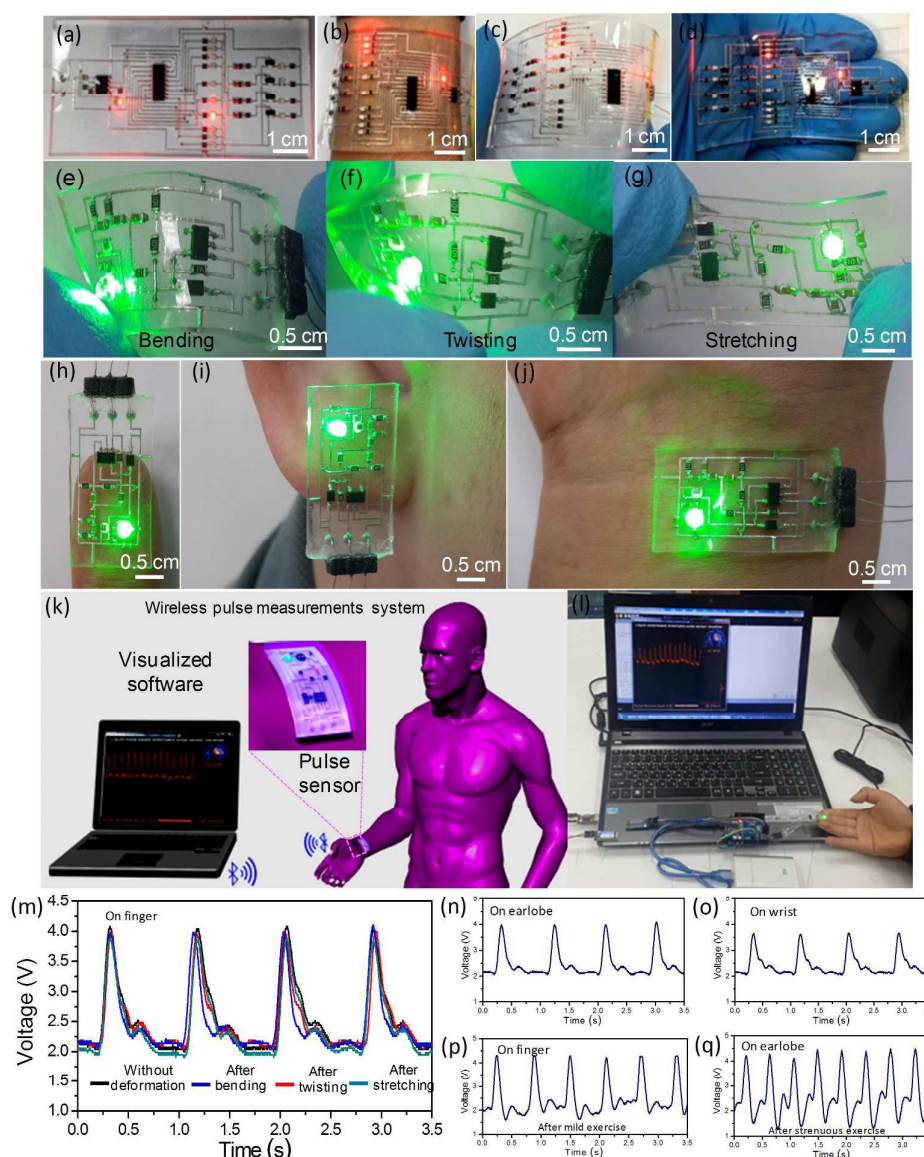


Fig.5. A transparent flowing LED light and a liquid-metal-based stretchable pulse sensor; (a) the top view of the transparent flowing LED light working under (b-g) various conditions include bending, twisting, stretching, etc. (h-i) The liquid-metal-based stretchable pulse sensor attached to various parts of the human body (finger, earlobe, and wrist). (k) Sketch of the wireless pulse-measurement system. (l) The wireless pulse-measurement system consists of the liquid-metal-based stretchable pulse sensor, a Bluetooth module, a computer, and self-programmed visualization software. (m-q) Measurement results of the human heart beating under various conditions when attached to the parts of human body.

width of 300 μm connected to electronic devices in the process of manufacturing the stretchable electronics. The LED circuit consists of an oscillator chip (NE555), a counter chip (CD40174), LED lights, diodes, resistors, and capacitors (circuit diagram shown in Fig. S4 of the ESI†). Fig. 5(b-d) reveals that the fabricated LED circuits are optically transparent, and exhibits excellent electrical and mechanical behaviors under arbitrary deformation. Moreover, it can be easily attached to the human skin thanks to the soft-elastic characteristics of PDMS material. An additional decrease in wire line width can be easily achieved by utilizing the aforementioned "S"-shaped patterns.

Finally, the improved SLMP technique is employed to fabricate the stretchable pulse sensor for personal health monitoring applications. After applying a 5-V DC power, the green LED light is turned on, and the stretchable pulse sensor works very well under arbitrary deformation (Fig. 5(e-g)). Fig. 5(h-j) show optical images of fabricated stretchable pulse sensors attached to various areas of human skin such as onto the finger, earlobe, and wrist. For non-invasive heart-rate monitoring in home health care, the stretchable pulse sensors are combined with a home-made wireless system. The wireless healthcare system consists of the fabricated pulse sensor, a Bluetooth module, an Arduino board, a laptop computer

and a home-made graphic user interface (GUI) (Fig. 5(k-i)). When the stretchable pulse sensor is attached to a person's skin, the electrical signal obtained from the sensor is converted to a digital signal using an Arduino board with a Bluetooth module. The digital signal is wirelessly transmitted to the laptop computer and then the results is displayed on a monitor (Video SV. 1 and SV. 2 of the ESI†). Fig. 5(m-q) show the experimental results of the stretchable pulse sensor attached to human skins. The attached pulse sensor showed stable performance even under various mechanical stimulations such as torsion, stretching etc. The pulse period also increased with the increase of the exercise, and the pulse shape and cycle were successfully visualized through the home-made GUI. These experimental results reveal that the stretchable pulse sensor exhibits excellent electrical and mechanical behaviors in any mechanical strain such as flexure, torsion, and stretching.

Conclusion

In this paper, a liquid-metal-based flexible and stretchable pulse sensor realized by the advanced SLMP technique has been introduced for personal healthcare applications. The fabricated pulse sensor fully covers human skin and monitors the patient's heartbeats in a simple and inexpensive way that is suitable for home healthcare. The propose SLMP technique is significantly improved the resolution and the uniformity of liquid-metal patterns with a minimum width of about 2 μm . After optimization of the fabrication processes, we verified the applicability of the advanced SLMP technique by realizing a transparent LED light with programmed circuits. Finally, the idea is utilized to realize the platform of the liquid-metal-based pulse sensor (integrated with a light source, photoelectric converter low-pass filter, and operational amplifier). The observed results reveal that the proposed pulse-measurement system is very convenient and comfortable for monitoring patients' heart rate. We believe that the portable non-invasive liquid-metal-based stretchable pulse sensor has great potential to improve patients' life.

Experimental Section

Preparation of liquid-metal

Galinstan is a commercially available (from Geratherm Medical AG, Germany) eutectic GaInSn metal alloy (68.5%, 21.5%, and 10% by weight, respectively) that exhibits outstanding properties such as a low melting point (-19°C), high electrical conductivity ($3.46 \times 10^6 \text{ Sm}^{-1}$), high boiling point (1300°C), favourable thermal conductivity ($16.5 \text{ Wm}^{-1}\text{K}^{-1}$), and an ultra-low vapor pressure that can exist in liquid phase at room temperature.

Fabrication of liquid-metal-based stretchable pulse sensor

Fig. 1 shows the fabrication process for the stretchable pulse sensor using the selective wetting behaviour of a reduced liquid-metal. An optically clear, inert, non-toxic, and non-flammable material known as PDMS solution was spin-coated on a Si wafer (800 rpm for 30 s) and then placed on a hot plate at 80°C for 90 min. After the curing process, the PDMS layer was exposed to oxygen plasma at 60 W for 90 s, which enhances the adhesion

ability between the metal and the PDMS. Next, a Au/Cr thin layer was deposited on the sample, and electrical circuits for a pulse sensor was obtained using conventional photolithography and Au/Cr wet-etching processes. Surface cracking occurs with a higher probability when oxygen plasma treatment is done before Cr / Au (10/100 nm) deposition on elastomer substrates (37, 38). This can be minimized by using the HMDS (Hexamethyldisiloxane) treatment, which is employed to enhance the adhesion ability between the metal and the PDMS layers (shown in Fig. S5 of the ESI†). Before Au/Cr metal deposition, the PDMS layer was placed in the HMDS vapor with sealed environment for 12 hours. Even if the surface cracking occurs, it has no influence to the liquid metal pattern. As shown in Fig. S6(a) of the ESI†, there is some surface cracking on Au patterns when the PDMS layer is treated with oxygen plasma. However, the metal surface cracking is disappeared after covered by a thin Cu using an electroplating technique as shown in Fig. S6(b) of the ESI†. Therefore, the surface cracking has no influence to the uniformity of liquid metal pattern shown in from Fig. S6(c) of the ESI†. This is due the liquid characteristics of the metallic material. After the wet-etching processes, the Au/Cr patterns were covered by a thin Cu using an electroplating technique. The thin metal patterns were then covered again using a liquid-metal droplet treated with a 37 wt% HCl solution. The reduced liquid-metal droplet was rolled over the patterns for 2 min, which ensures that the reduced liquid metal full wets the patterned Cu layer. Finally, the remainder of the reduced liquid-metal was removed from the circuits. After rinsing with an acetone solution, the liquid metal circuit pattern was treated with isopropyl alcohol (IPA) and placed on a hot plate at 60°C for 5 min. The electronic elements (including an optical receiver (APDS-9008), LED, operational amplifier chip (MCP6001), diodes, resistors, and capacitors) were then integrated on liquid metal wires to realize a functional circuit. After integration, the sensor circuit was covered with a PDMS solution and placed on a hot plate at 60°C for 4 h. After curing, the Si substrate was removed to release the stretchable sensor embedded in PDMS.

Acknowledgements

This study was supported by the National Research Foundation Grant (No. 2015R1A2A2A05001405) and Commercialization Promotion Agency for R&D Outcomes (COMPA) funded by the Ministry of Science, ICT and Future Planning (MSIP) (No.2016K000209). It was also partially supported by the china Postdoctoral Science Foundation (No. 2017M611963) and Talent Planning Project (No.ZX2017000230).

References

1. T. Gao, J. Liao, J. Wang, Y. Qiu, Q. Yang, M. Zhang, Y. Zhao, L. Qin, H. Xue and Z. Xiong, *J. Mater. Chem. A* 2015, **3**, 9965–9971.
2. C.-S. Hu, Y.-F. Chung, C.-C. Yeh and C.-H. Luo, *J. Evidence-Based Complementary Altern. Med.* 2011, **2012**, 745127.
3. Y. Jiang, H. Hamada, S. Shiono, K. Kanda, T. Fujita, K. Higuchi and K. Maenaka, *Procedia Eng.* 2010, **5**, 1466–1469.

4. Y. Wang, L. Wang, T. Yang, X. Li, X. Zang, M. Zhu, K. Wang, D. Wu and H. Zhu, *Adv. Funct. Mater.* 2014, **24**, 4666–4670.
5. X. Chen, J. Shao, N. An, X. Li, H. Tian, C. Xu and Y. Ding, *J. Mater. Chem. C* 2015, **3**, 11806–11814.
6. C. Pang, J. H. Koo, A. Nguyen, J. M. Caves, M.-G. Kim, A. Chortos, K. Kim, P. J. Wang, J. B.-H. Tok and Z. Bao, *Adv. Mater.* 2015, **27**, 634–640.
7. G. Zhu, W. Q. Yang, T. Zhang, Q. Jing, J. Chen, Y. S. Zhou, P. Bai and Z. L. Wang, *Nano Lett.* 2014, **14**, 3208–3213.
8. L. Gao, Y. Zhang, V. Malyarchuk, L. Jia, K.-I. Jang, R. C. Webb, H. Fu, Y. Shi, G. Zhou, L. Shi, D. Shah, X. Huan, B. Xu, C. Yu, Y. Huang and J. A. Rogers, *Nat. Commun.* 2014, **5**, 4938.
9. M. S. Manno, H. Tao, J. D. Clayton, A. Sengupta, D. L. Kaplan, R. R. Naik, N. Verma, F. G. Omenetto and M. C. McAlpine, *Nat. Commun.* 2012, **3**, 763.
10. M. D. Dickey, *Adv. Mater.* 2017, 1606425 (1-19).
11. S. Gong, W. Schwalb, Y. Wang, Y. Chen, Y. Tang, J. Si, B. Shirinzadeh and W. Cheng, *Nat. Commun.* 2014, **5**, 1–8.
12. A. J. Bandodkar, I. Jeerapan, J. You, R. Nuñez-Flores and J. Wang, *Nano Lett.* 2016, **16**, 721–727.
13. M. Amjadi, A. Pichitpajongkit, S. Lee, S. Ryu, and I. Park, *ACS Nano* 2014, **8**, 5154–5163.
14. S.H. Jeong, A. Hagman, K. Hjort, M. Jobs, J. Sundqvist and Z.G. Wu, *Lab Chip* 2012, **12**, 4657–4664.
15. S. H. Jeong, K. Hjort and Z. G. Wu, *Sensors* 2014, **14**, 16311–16321.
16. S. Cheng and Z. G. Wu, *Lab Chip* 2010, **10**, 3227–3234.
17. C. Fassler and C. Majidi, *Smart Mater. Struct.* 2013, **22**, 055023-1–055023-8.
18. E. Palneau, S. Reece, S. C. Desai, M. E. Smith and M. D. Dickey, *Adv. Mater.* 2013, **25**, 1589–1592.
19. K. Khoshmanesh, S. Tang, J. Y. Zhu, S. Schaefer, A. Mitchell, K. Kalantar-zadeh and M. D. Dickey, *Lab Chip* 2017, **17**, 974–993.
20. S. Zhu, J.-H. So, R. Mays, S. Desai, W. R. Barnes, B. Pourdeyhi and M. D. Dickey, *Adv. Funct. Mater.* 2013, **23**, 2308–2314.
21. S. H. Jeong, K. Hjort, Z. G. Wu, *Sci. Rep-Uk*. 2015, **5**, 08419-1–08419-7.
22. Q. Zhang, Y. Gao and J. Liu, *Appl. Phys. A-Mater.* 2014, **116**, 1091–1097.
23. L. Wang and J. Liu, *RSC Adv.* 2015, **5**, 57686–57691.
24. Y. Gao, H. Li, J. Liu, *PLOS ONE* 2012, **7**, e45458-1–e45458-10.
25. Y. Zheng, Z. He, Y. Gao and J. Liu, *Sci. Rep-Uk*. 2013, **3**, 01786-1–01786-7.
26. A. Tabatabai, A. Fassler, C. Usiak and C. Majidi, *Langmuir* 2013, **29**, 6194–6200.
27. C. Ladd, J. So, J. Muth and M.D. Dickey, *Adv. Mater.* 2013, **25**, 5081–5085.
28. J.W. Boley, E.L. White, G.T.-C. Chiu and R. K. Kramer, *Adv. Funct. Mater.* 2014, **24**, 3501–3507.
29. Y. Zheng, Z. Z. He, J. Yang and J. Liu, *Sci. Rep-Uk*. 2014, **4**, 04588-1–04588-8.
30. R.K. Kramer, C. Majidi and R. J. Wood, *Adv. Funct. Mater.* 2013, **23**, 5292–5296.
31. G. Li, X. Wu and D.-W. Lee, *Lab chip* 2016, **16**, 1366–1373.
32. G. Li, M. Parmar and D.-W. Lee, Nanotechnology (IEEE-NANO), 2013 13th IEEE Conference on 2013, 410 – 413.
33. G. Li, M. Parmar, D. Kim, J.-B. Lee and D.-W. Lee, *Lab chip* 2014, **14**, 200–209.
34. G. Li, M. Parmar and D.-W. Lee, *Lab chip* 2015, **15**, 766–775.
35. G. Li, X. Wu and D.-W. Lee, Solid-State Sensors, Actuators and Microsystems (TRANSDUCERS), 2015 Transducers - 2015 18th International Conference on 2015, 339–342.
36. G. Li, X. Wu and D.-W. Lee, *Sensor Actuat B-Chem.* 2015, **221**, 1114–1119.
37. O. Graudejus, P. Görrn and S. Wagner, *ACS Appl. Mater. Interfaces* 2010, **2**, 1927–1933.
38. C. Huang, J. Lv, X. Tian, Y. Wang, Y. Yu and J. Liu, *Sci. Rep.*, 2015, **5**, 14787.